Modelling of divertor plasma transport in stochastic magnetic boundary

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Role of SOL plasma in fusion reactor

Confinement region:

~10keV, 10^{20} m⁻³, α -particle confinement/heating control of pressure/current profile, 500MW fusion power, Q>10

Power through LCFS

Impurity, fuel influx

Scrape-off layer:

1~few hundreds eV, 10^{20} ~ 10^{21} m⁻³, balance between // & _____ transport, power removal with radiation, impurity transport (material migration), plasma flow distribution, interaction with neutrals

Power/particle flux



Fuel recycling, impurity source

Material surface: divertor target, first wall plasma neutralization, erosion, deposition, fuel retention, heat removal & fuel/He ash pumping

Mitigation of power load on divertor plate
Reduction of Impurity influx to confinement region
High pumping efficiency of fuel, He ash



Motivation

Stochastic field as a tool for controlling edge plasma

RMP for ELMs mitigation

RMP reduces pressure gradient, interacts with eigenmode structure of ELMs



e.g. Ergodic divertor in
TEXT, Tore Supra,
TEXTOR-DED etc.
→ enhanced radial transport,
edge radiation, impurity
screening etc.



Intrinsic edge stochastization in Heliotron configuration

Understanding of plasma transport characteristics in stochastic field is inevitable for divertor optimization



Symmetry breaking by Resonant Magnetic Perturbation 2D axi-symmetric → 3D non-axi-symmetric

Controllability of edge plasma for divertor optimization

Study on plasma transport in stochastic field

Magnetic field structure

Island formaion, overlap (vacuum approximation)

← plasma response

(field amplification, rotational screening, neoclassical effect)

Measurements

 \leftarrow magnetic probe outside plasma, T_e profile

Ideal stochastization

← quasi-linear model, diffusive picture

Realistic field

← mixture of remnant islands, local ergodic

field, laminar region

Contents of the talk

- 1. Formation of magnetic island and stochastic field
- 2. Realistic field structure in devices
- 3. Effects on transport (3D treatment)
 - --- divertor plasma parameters
 - --- SOL impurity transport
- 4. Summary
 - --- further topics to be addressed

Transport analysis

Analytical formulae (e.g. R-R model)

 // & __ transport interplay (3D treatment)
 <u>Time averaged field</u> EMC3-EIRENE, E3D, FINDIF etc.
 <u>Fluctuating field</u> Electrostatic/electromagnetic turbulence (P. Beyer et al., DALF3) etc.

1. Formation of magnetic island and stochastic field

Formation of magnetic island : vacuum field



Onset of stochastic instability by island overlapping: σ_{Chir} > 1



ITER International Summer School 2009, 22-26 June 2009, Aix en Provence, France K.H. Finken et al., "The structure of magnetic field in the TEXTOR-DED"

Field line structure in stochastic magnetic boundary



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Connection length (L_c) distribution in TEXTOR-DED



3. Effects on transport (3D treatment)

Magnetic field structure in LHD (Large Helical Device)



3D modelling of LHD edge region (EMC3-EIRENE)

Computational mesh, configuration and installations

Core, CX-neutral transport, particle source
 SOL, EMC3 simulation domain
 Vacuum of plasma*

Physics model

Standard fluid equations of mass, momentum, ion and electron energy
Trace impurity fluid model (Carbon)
Kinetic model for neutral gas (Eirene)

Boundary conditions

- •Bohm condition at divertor plates
- •Power entering the SOL
- •Density on LCMS
- Sputtering coefficient

Cross-field transport coefficients

χ_e=χ_i=3D roughly holds
 spatially constant (global transport)
 determined experimentally



Model equations in EMC3-EIRENE

Background plasma (fluid):

 $\nabla \cdot (n_i V_{i||} \boldsymbol{b} - D \boldsymbol{b}_{\perp} \boldsymbol{b}_{\perp} \cdot \nabla n_i) = S_p$ $\nabla \cdot (m_i n_i V_{i||} V_{i||} \boldsymbol{b} - \eta_{||} \boldsymbol{b} \boldsymbol{b} \cdot \nabla V_{i||} - m_i V_{i||} D \boldsymbol{b}_{\perp} \boldsymbol{b}_{\perp} \cdot \nabla n_i - \eta_{\perp} \boldsymbol{b}_{\perp} \boldsymbol{b}_{\perp} \cdot \nabla V_{i||}) = -\boldsymbol{b} \cdot \nabla p + S_m$ $\nabla \cdot (\frac{5}{2} n_e T_e V_{i||} \boldsymbol{b} - \kappa_e \boldsymbol{b} \boldsymbol{b} \cdot \nabla T_e - \frac{5}{2} T_e D \boldsymbol{b}_{\perp} \boldsymbol{b}_{\perp} \cdot \nabla n_e - \chi_e n_e \boldsymbol{b}_{\perp} \boldsymbol{b}_{\perp} \cdot \nabla T_e) = -k(T_e - T_i) + S_{ee} + S_{imp}$ $\nabla \cdot (\frac{5}{2} n_i T_i V_{i||} \boldsymbol{b} - \kappa_i \boldsymbol{b} \boldsymbol{b} \cdot \nabla T_i - \frac{5}{2} T_i D \boldsymbol{b}_{\perp} \boldsymbol{b}_{\perp} \cdot \nabla n_i - \chi_i n_i \boldsymbol{b}_{\perp} \boldsymbol{b}_{\perp} \cdot \nabla T_i) = +k(T_e - T_i) + S_{ei}$

Impurities (fluid):

$$\nabla \cdot \left(n_{I}^{z} V_{III}^{z} \boldsymbol{b} - D_{I}^{z} \boldsymbol{b}_{\perp} \boldsymbol{b}_{\perp} \cdot \nabla n_{I}^{z} \right) = S_{z-l \to z} - S_{z \to z+l} + R_{z+l \to z} - R_{z \to z-l}$$

$$U_{Ii}^{z} \left(V_{III}^{z} - V_{iII} \right) = -\boldsymbol{b} \cdot \nabla n_{I}^{z} T_{I}^{z} + n_{I}^{z} Z e E_{II} + n_{I}^{z} Z^{2} C_{e} \boldsymbol{b} \cdot \nabla T_{e} + n_{I}^{z} C_{i} \boldsymbol{b} \cdot \nabla T_{e}$$

$$\boldsymbol{b} \cdot \nabla n_{e} T_{e} + n_{e} e E_{II} + n_{e} C_{e} \boldsymbol{b} \cdot \nabla T_{e} = 0$$

$$T_{I}^{z} = T_{i}$$

Neutrals (kinetic): Boltzmann equation (Eirene code)

Plasma-surface and neutral-surface interaction:

Particle and energy reflection, sputtering (Eirene code)



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Jump step of Monte Carlo particle

Fokker-Planck form

 $\nabla_{\parallel} \cdot \left[\mathbf{a}_{\parallel} f - \nabla_{\parallel} (b_{\parallel} f) \right] + \nabla_{\perp} \cdot \left[\mathbf{a}_{\perp} f - \nabla_{\perp} (b_{\perp} f) \right] = S,$

f:	density n	velocity \mathbf{V}_{\parallel}	temperature $T_{i,e}$
\mathbf{a}_{\parallel} :	V_{\parallel}	$m_i n V_{\ } + \nabla_{\ } \eta_{\ }$	$\frac{5}{2}nV_{\parallel} + \nabla_{\parallel}\kappa_{i,e}$
b_{\parallel} :	0	η_{\parallel}	$\kappa_{i,e}$
\mathbf{a}_\perp :	0	0	$(\chi_{i,e} - \frac{5}{2}D)\nabla_{\perp}n$
b_{\perp} :	D	$m_i n D$	$n\chi_{i,e}$
S:	S_p	$-\nabla_{\parallel} p + S_m$	$\pm k(T_e - T_i) + S_{ei,ee}$

<Coefficients for different f's>



3. Effects on transport (3D treatment) 3.1 divertor plasma parameters

Role of pressure conservation along flux tubes on T_{div}, n_{div}

Divertor plasma parameter in ASDEX



X-point divertor tokamaks

Pressure conservation along flux tube,

 $\nabla_{//}(nT+m_i nV_{//}^2)=0$

gives rise to sensitive divertor parameter dependence on upstream density :

High recycling regime (conduction limited regime)

$$n_{div} \propto n_{up}^{3} \qquad T_{div} \propto n_{up}^{-2}$$

The dependence is experimentally confirmed.

Stochastic boundary

The 3D flux tube geometry can introduce perpendicular terms \rightarrow breaking down of the pressure conservation.

$$\nabla_{//}(nT+m_inV_{//}^2)-\nabla_{\perp}(m_iV_{//}D_{\perp}\nabla_{\perp}n+\eta_{\perp}\nabla_{\perp}V_{//})=0$$





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Two point model with momentum loss in perpendicular direction





Divertor probe measurements confirm absence of high recycling regime prior to detachment



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$$T_d \propto P_{SOL}^{10/7} n_u^{-2} (1+f_m)^2,$$

$$n_d \propto P_{SOL}^{-8/7} n_u^{-3} (1+f_m)^{-3}$$

 Moderate dependence of T_{ed} & n_{ed} on n_u (T>10eV ← no significant CX loss, v_{SOL}*=L_c/mfp>10)
 >n_{ed} never exceeds upstream density

 ➢ Both 3D modellings & the two point model (with P_{SOL} variation due to NBI heating included) reproduce the experimental results.
 → effect of momentum loss via ⊥ interaction

Momentum loss via friction between counter flows in W7-AS/X



Field line geometry near divertor, $l_{l/l}$, δ_m , provides controllability of divertor regime.

Summary of 3.1 Divertor plasma parameters

- 1. $nV_{//}$ in stochastic boundary \rightarrow alternating flow regulated by remnant islands
- 2. n_{div} & T_{div} in stochastic boundary of LHD show modest sensitivity to n_{up}, in contrast to the high recycling regime in tokamaks.
- 3. Breakdown of parallel pressure conservation via perpendicular frictional interaction of the counter flows.
- 4. The degree of momentum loss can be described as $f_m \propto \frac{l_{//}}{T_a^{0.5} \delta_m^{-2}}$
- 5. The analysis in W7-AS, X

→ controllability of divertor regime: $n_d \propto n_u^3 \iff n_d \propto n_u^{1\sim 1.5}$

6. For future devices, $l_{l/}$, δ_m should be optimized for control of divertor plasma with stochastic magnetic field.

3. Effects on transport (3D treatment) 3.2 SOL impurity transport

3D impurity transport model : EMC3-EIRENE (fluid approximation)



 D_z is set to be the same value of bulk plasma that is deduced from experiments.



From thermal-force to friction-dominated impurity transport

Carbon density profiles by 3D model show impurity retention at high density



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Increasing density

- Enhances friction force in edge surface layer with flow acceleration by short flux tubes
- → Stops carbon penetration in edge surface layers
- ➔ Feels more friction
- Suppresses thermal force in stochastic region





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Key role of remnant islands on impurity transport





$$\nabla_{\prime\prime}T_i \approx -\frac{q_r \Theta}{n\chi_{\perp}} \propto n^{-1}$$

Increasing density suppresses //-T gradient, i.e. thermal force in the presence of remnant islands.

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Radial profiles of each charge states of carbon density

Impurity screening \rightarrow shift of impurity density profile to low temperature region



Emission measurements in experiments indicate impurity retention potential at high density



Signature of impurity screening with stochastic boundary various devices



C⁶⁺ density in confinement region decreases with increasing density.

C⁶⁺ concentration in core region decreases with DED activation.

Summary: SOL Impurity transport

1. 3D impurity transport modelling in the stochastic magnetic structure shows impurity screening effect at high density :

Increasing density

- Enhances friction force in edge surface layer with flow acceleration by rich ionization source
- → Stops carbon penetration in edge surface layers → Feels more friction
- → Suppresses thermal force in stochastic region
- 2. The remnant islands with small $\Theta (\approx w/l_{//})$, $\frac{n\chi_{\perp}}{\kappa_{i0}T_{i}^{2.5}} >> \Theta^{2}$ and high density $\rightarrow \nabla_{//}T \propto n^{-1}$

i.e. suppression of thermal force at high density

3. The edge carbon emission measurements agree well with the code results, indicating impurity retention effect of stochastic magnetic boundary.

Summary

Plasma transport in stochastic magnetic boundary in LHD is analyzed by the 3D edge transport code in comparison with experimental results and with other devices.

1. Magnetic shear + RMP

 \rightarrow topological change of field lines (magnetic island), stochastic instability

→ \bot , // characteristic scale: $\delta_{\rm m},$ w, $\,l_{\!_{/\!/}}$

2. Influence on divertor regime:

high recycling \leftrightarrow > no high recycling with $f_m \propto \frac{l_{//}}{T_r^{0.5} \delta^{-2}}$

3. Impurity screening potential at high density with very small $\Theta (\approx w/l_{//})$, $\frac{n\chi_{\perp}}{\kappa_{i0}T_i^{2.5}} >> \Theta^2$ and flow acceleration in edge surface layers (laminar region).

These geometrical parameters provide control of edge plasma transport in stochastic SOL.

Stochastic magnetic boundaries

→Symmetry breaking

 \rightarrow Controllability of edge plasma transport

<u>Further topics to be investigated</u> Power load dispersal on divertor plates Plasma response to RMP. Electric field formation, determination of D,D_Z, χ . Quantitative estimation for future devices

Field lines connect divertor plate with different connection lengths (ranges in two orders, 10 m ~ 1000 m) >Magnetic shear + \widetilde{B}_r > stretching, bending, compression of flux tubes $\widetilde{B}_{...}$ l(s) $\leq \sqrt[4]{\delta(s)}$ Magnetic shear L_c profiles on divertor plates _____ 90 $L_{c}(m)$ 2.695+03 7.27E+03 The long & short flux tubes 1.15E + 033.10**b**low up are mixed due to the 85 4.89E+02 deformation, creating fine 1.32Estructure. 2.09E+02 5.64E+02 theta (deg) 8.906+01 2.41E+02 Not only //, BUT ⊥ energy ~4 cm 80 0 exchange between flux 3.80E+01 1.03E+02 tubes plays important role 1.62E + 014.38E+01 in determining wetted area. 1.87E+01 6.91E+00 75 -100 7.98E+00 2.95E+00 3.41E+00 1.260 + 0070 20 30 Ο 10 40 2 3 4 5 6 phi (deq) phi (dea)

3D Modelling : Power deposition profile insensitive to P_{SOL}



PROBE10.5U_P02_D0.50_1.50_NUP4

Maximum power load linearly scales with P_{SOL} , indicating no P_{SOL} dependence of Δ_{energy} .

Because of $\Delta_{energy} >> \lambda_p$, change of λ_p is negligible.

IR camera measurements in TEXTOR-DED: Divertor heat flux is well correlated with L_c distribution



M. Jakubowski et al., PPCF 49 (2007) S109.

Plasma response to RMP : screening/amplification by current induced around resonance surface



Y. Kikuchi et al. NF 44 (2004) S28.

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Neo-classical effect : bootstrap current, polarization current





Figure 7. $\beta - \nu_h^*$ space. (*a*) Open circles indicate the cases where the island is not observed. Closed circles denote that the island is observed. (*b*) The $\beta - \nu_h^*$ space made from the acquired data in [3].

Y. Narushima et al., Nucl. Fusion **48** (2008) 075010.

N. Ohyabu et al., Phys. Rev. Lett. 88 (2002) 055005. 39

K. Itoh, S.I. Itoh and M. Yagi, Phys. Plasmas 12 (2005) 072512.

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Possibility for stable detachment control with remnant island structure



Strong radiation is localized at the remnant island structure

Y. Feng et al., NF 48 (2008) 024012.

Interaction of island chain of different modes at high field region leads to strong flow shear → Momentum loss via cross-field friction





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Summary of 3.1 Divertor plasma parameters

What we have learned

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- 3. Breakdown of parallel pressure conservation via perpendicular frictional interaction of the counter flows.
- 4. The degree of momentum loss can be described as $f_m \propto \frac{l_{//}}{T_{\star}^{0.5} \delta^{-2}}$
- 5. The analysis in W7-AS, X
 - \rightarrow controllability of divertor regime: $n_d \propto n_u^3 \leftrightarrow n_d \propto n_u^{1\sim 1.5}$
- 6. For future devices, $l_{l,l}, \delta_m$ should be optimized for control of divertor plasma. e.g. for good neutral compression, f_m should be small.

What we haven't yet understood

- 1. If D has parameter dependence, $f_m(n_d, T_d)$? \rightarrow affects *qualitative* dependence!!
- 2. If \perp momentum flux is not $\propto \nabla_{\perp} n V_{//}$, but convective one $\propto V_{\perp,conv} V_{//}$ then $f_m \propto \frac{l_{//}}{\delta_m}$? → affects *quantitative* dependence!

Summary: SOL Impurity transport

What we haven't yet understood

- 1. Parameter & Z dependence of $D_{Z^{\perp}}$? \rightarrow affects *quantitative* dependence!
- 2. \perp convective term $\Theta V_{Z//} + V_{Z,conv}$? \rightarrow affects *qualitative* dependence!!

Simplified // force balance between friction and ion thermal for

1D radial continuity,

Ind ion thermal force reads,

$$V_{Z/I} = V_{I/I} + C_{I} \frac{\tau_{ZI}}{m_{Z}} Z^{2} \nabla_{I/I} T_{I}$$

$$\sum_{Z} \rightarrow \frac{d}{dr} \left(\Theta n_{Z} V_{Z/I} - D_{Z\perp} \frac{dn_{Z}}{dr} \right) = -S_{Z} - R_{Z} + S_{Z-1} + R_{Z+1}$$

$$\sum_{Z} \rightarrow \frac{d}{dr} \left(\Theta n_{I} V_{Z/I} - D_{Z\perp} \frac{dn_{I}}{dr} \right) = 0$$
Solution for target-released impurities:

$$n_{I,LCMS} / n_{I,target} = \exp \left(-\int_{LCMS}^{target} \frac{\Theta V_{Z/I}}{D_{Z\perp}} dr \right) \qquad \frac{n_{I,LCMS}}{n_{I,target}} \prod_{V_{Z/I} > 0}^{V_{Z/I} > 0}$$

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 $n_{I,LCMS}$





